



**ΕΛΛΗΝΙΚΗ ΔΗΜΟΚΡΑΤΙΑ  
ΠΑΝΕΠΙΣΤΗΜΙΟ ΚΡΗΤΗΣ**

# **Ψηφιακή Επεξεργασία Φωνής**

**Ενότητα 3η: Ακουστική Ανάλυση Παραγωγής  
Φωνής**

**Στυλιανού Ιωάννης**

**Τμήμα Επιστήμης Υπολογιστών**

# CS578- SPEECH SIGNAL PROCESSING

## LECTURE 3: ACOUSTICS OF SPEECH PRODUCTION

Yannis Stylianou



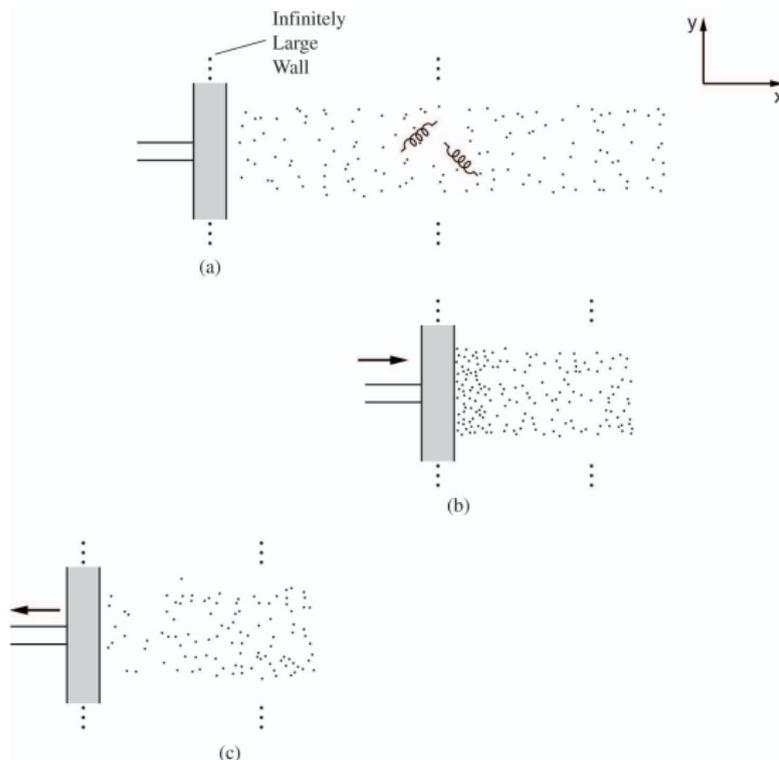
University of Crete, Computer Science Dept., Multimedia Informatics Lab  
yannis@csd.uoc.gr

Univ. of Crete, 2008 Winter Period

# OUTLINE

- 1 PHYSICS OF SOUND
- 2 UNIFORM TUBE MODEL
- 3 CONCATENATING N UNIFORM TUBES
- 4 GLOTTAL FLOW DERIVATIVE
- 5 VOCAL FOLD/VOCAL TRACT INTERACTION
- 6 ACKNOWLEDGMENTS
- 7 REFERENCES

# COMPRESSION AND RAREFACTION OF AIR PARTICLES



# SOME DEFINITIONS

- **Sound wave:** propagation of disturbance (local changes in pressure, displacement, and velocity) of particles through a medium, creating the effect of compression or rarefaction.
- **Wavelength:** distance between two consecutive peak compressions,  $\lambda$
- **Frequency:** number of cycles of compressions per second,  $f$
- **Speed of sound:**  $c = f\lambda$  (at sea level and at  $70^{\circ}F$ ,  $c = 344m/sec$ )
- **Isothermal process:** a slow variation of pressure where the temperature in the medium remains constant
- **Adiabatic process:** a fast variation of pressure where the temperature in the medium increases

# SOME DEFINITIONS

- **Sound wave:** propagation of disturbance (local changes in pressure, displacement, and velocity) of particles through a medium, creating the effect of compression or rarefaction.
- **Wavelength:** distance between two consecutive peak compressions,  $\lambda$
- **Frequency:** number of cycles of compressions per second,  $f$
- **Speed of sound:**  $c = f\lambda$  (at sea level and at  $70^\circ F$ ,  $c = 344m/sec$ )
- **Isothermal process:** a slow variation of pressure where the temperature in the medium remains constant
- **Adiabatic process:** a fast variation of pressure where the temperature in the medium increases

# SOME DEFINITIONS

- **Sound wave:** propagation of disturbance (local changes in pressure, displacement, and velocity) of particles through a medium, creating the effect of compression or rarefaction.
- **Wavelength:** distance between two consecutive peak compressions,  $\lambda$
- **Frequency:** number of cycles of compressions per second,  $f$
- **Speed of sound:**  $c = f\lambda$  (at sea level and at  $70^\circ F$ ,  $c = 344m/sec$ )
- **Isothermal process:** a slow variation of pressure where the temperature in the medium remains constant
- **Adiabatic process:** a fast variation of pressure where the temperature in the medium increases

# SOME DEFINITIONS

- **Sound wave:** propagation of disturbance (local changes in pressure, displacement, and velocity) of particles through a medium, creating the effect of compression or rarefaction.
- **Wavelength:** distance between two consecutive peak compressions,  $\lambda$
- **Frequency:** number of cycles of compressions per second,  $f$
- **Speed of sound:**  $c = f\lambda$  (at sea level and at  $70^\circ F$ ,  $c = 344m/sec$ )
- **Isothermal process:** a slow variation of pressure where the temperature in the medium remains constant
- **Adiabatic process:** a fast variation of pressure where the temperature in the medium increases

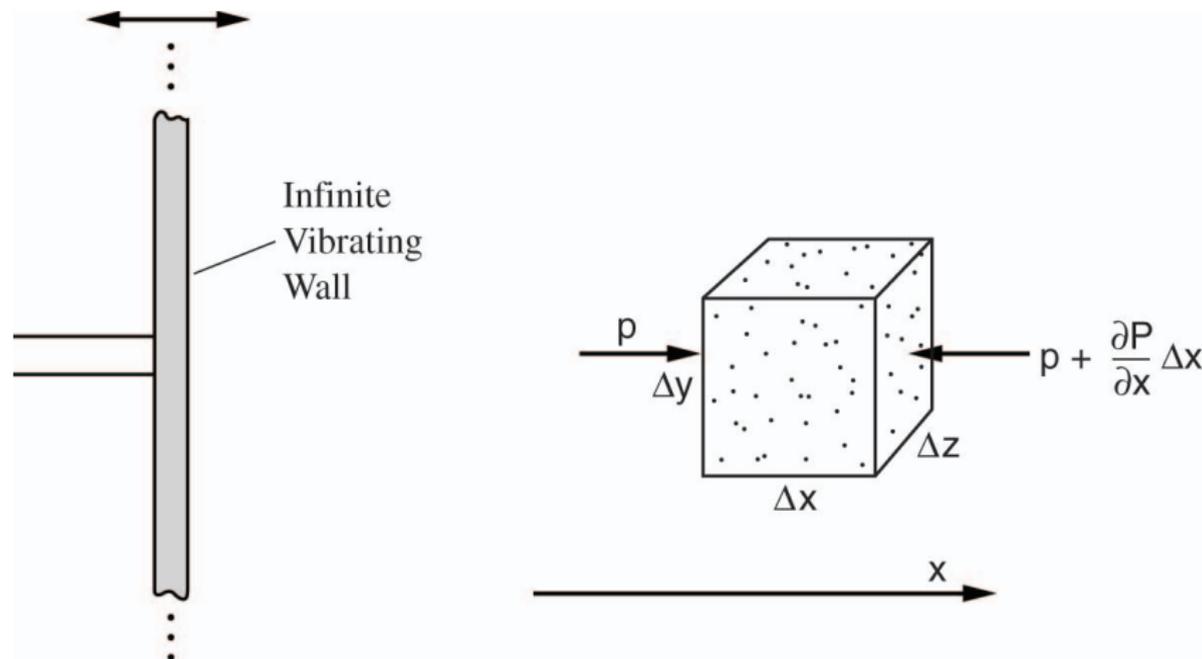
# SOME DEFINITIONS

- **Sound wave:** propagation of disturbance (local changes in pressure, displacement, and velocity) of particles through a medium, creating the effect of compression or rarefaction.
- **Wavelength:** distance between two consecutive peak compressions,  $\lambda$
- **Frequency:** number of cycles of compressions per second,  $f$
- **Speed of sound:**  $c = f\lambda$  (at sea level and at  $70^\circ F$ ,  $c = 344m/sec$ )
- **Isothermal process:** a slow variation of pressure where the temperature in the medium remains constant
- **Adiabatic process:** a fast variation of pressure where the temperature in the medium increases

# SOME DEFINITIONS

- **Sound wave:** propagation of disturbance (local changes in pressure, displacement, and velocity) of particles through a medium, creating the effect of compression or rarefaction.
- **Wavelength:** distance between two consecutive peak compressions,  $\lambda$
- **Frequency:** number of cycles of compressions per second,  $f$
- **Speed of sound:**  $c = f\lambda$  (at sea level and at  $70^\circ F$ ,  $c = 344m/sec$ )
- **Isothermal process:** a slow variation of pressure where the temperature in the medium remains constant
- **Adiabatic process:** a fast variation of pressure where the temperature in the medium increases

# CUBE CONFIGURATION



# NOTATION

Assuming *planar propagation*, and within the cube:

- $p(x, t)$  fluctuation of pressure about an ambient or average pressure  $P_0$ .
  - ▷ Threshold of hearing:  $2 \cdot 10^{-5}$  newtons/m<sup>2</sup>
  - ▷ Threshold of pain: 20 newtons/m<sup>2</sup>
- $v(x, t)$  fluctuation of particles' velocity about zero average velocity.
- $\rho(x, t)$  fluctuation of particles' density about an average density  $\rho_0$ .

# NOTATION

Assuming *planar propagation*, and within the cube:

- $p(x, t)$  fluctuation of pressure about an ambient or average pressure  $P_0$ .
  - ▷ Threshold of hearing:  $2 \cdot 10^{-5}$  newtons/m<sup>2</sup>
  - ▷ Threshold of pain: 20 newtons/m<sup>2</sup>
- $v(x, t)$  fluctuation of particles' velocity about zero average velocity.
- $\rho(x, t)$  fluctuation of particles' density about an average density  $\rho_0$ .

# NOTATION

Assuming *planar propagation*, and within the cube:

- $p(x, t)$  fluctuation of pressure about an ambient or average pressure  $P_0$ .
  - ▷ Threshold of hearing:  $2 \cdot 10^{-5}$  newtons/m<sup>2</sup>
  - ▷ Threshold of pain: 20 newtons/m<sup>2</sup>
- $v(x, t)$  fluctuation of particles' velocity about zero average velocity.
- $\rho(x, t)$  fluctuation of particles' density about an average density  $\rho_0$ .

# THE WAVE EQUATION

Under the assumptions:

- If there is no friction of air particles in the cube with those outside the cube (no *viscosity*),
- Cube is very small,
- The density of air particles is constant in the cube (i.e.,  $\rho_0 = \rho$ )

then, one form of the *Wave Equation* is given by:

$$\begin{aligned} -\frac{\partial p}{\partial x} &= \rho \frac{\partial v}{\partial t} \\ -\frac{\partial p}{\partial t} &= \rho c^2 \frac{\partial v}{\partial x} \end{aligned}$$

# THE WAVE EQUATION

Under the assumptions:

- If there is no friction of air particles in the cube with those outside the cube (no *viscosity*),
- Cube is very small,
- The density of air particles is constant in the cube (i.e.,  $\rho_0 = \rho$ )

then, one form of the *Wave Equation* is given by:

$$\begin{aligned} -\frac{\partial p}{\partial x} &= \rho \frac{\partial v}{\partial t} \\ -\frac{\partial p}{\partial t} &= \rho c^2 \frac{\partial v}{\partial x} \end{aligned}$$

# THE WAVE EQUATION

Under the assumptions:

- If there is no friction of air particles in the cube with those outside the cube (no *viscosity*),
- Cube is very small,
- The density of air particles is constant in the cube (i.e.,  $\rho_0 = \rho$ )

then, one form of the *Wave Equation* is given by:

$$\begin{aligned} -\frac{\partial p}{\partial x} &= \rho \frac{\partial v}{\partial t} \\ -\frac{\partial p}{\partial t} &= \rho c^2 \frac{\partial v}{\partial x} \end{aligned}$$

# THE WAVE EQUATION

Under the assumptions:

- If there is no friction of air particles in the cube with those outside the cube (no *viscosity*),
- Cube is very small,
- The density of air particles is constant in the cube (i.e.,  $\rho_0 = \rho$ )

then, one form of the *Wave Equation* is given by:

$$\begin{aligned} -\frac{\partial p}{\partial x} &= \rho \frac{\partial v}{\partial t} \\ -\frac{\partial p}{\partial t} &= \rho c^2 \frac{\partial v}{\partial x} \end{aligned}$$

# THE WAVE EQUATION

Under the assumptions:

- If there is no friction of air particles in the cube with those outside the cube (no *viscosity*),
- Cube is very small,
- The density of air particles is constant in the cube (i.e.,  $\rho_0 = \rho$ )

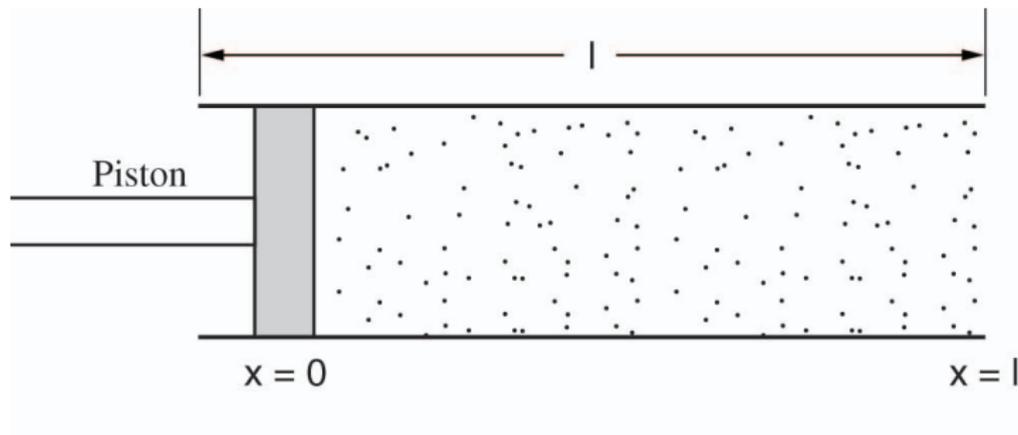
then, one form of the *Wave Equation* is given by:

$$\begin{aligned} -\frac{\partial p}{\partial x} &= \rho \frac{\partial v}{\partial t} \\ -\frac{\partial p}{\partial t} &= \rho c^2 \frac{\partial v}{\partial x} \end{aligned}$$

# OUTLINE

- 1 PHYSICS OF SOUND
- 2 UNIFORM TUBE MODEL**
- 3 CONCATENATING N UNIFORM TUBES
- 4 GLOTTAL FLOW DERIVATIVE
- 5 VOCAL FOLD/VOCAL TRACT INTERACTION
- 6 ACKNOWLEDGMENTS
- 7 REFERENCES

# LOSSLESS CASE OF CROSS SECTION A



$$\begin{aligned} -\frac{\partial p}{\partial x} &= \frac{\rho}{A} \frac{\partial u}{\partial t} \\ -\frac{\partial p}{\partial t} &= \frac{\rho c^2}{A} \frac{\partial u}{\partial x} \end{aligned}$$

where  $u(x, t) = Av(x, t)$

# SOLUTION FOR A LOSSLESS TUBE

Under the assumptions/conditions:

- No friction along the walls of the tube
- At the open end of the tube, there are no variations in air pressure, i.e.  $p(l, t) = 0$
- Volume velocity at  $x = 0$ :  $u(0, t) = U_g(\Omega)e^{j\Omega t}$

▷ Volume velocity:

$$u(x, t) = \frac{\cos[\Omega(l-x)/c]}{\cos(\Omega l/c)} U_g(\Omega)e^{j\Omega t}$$

▷ (Incremental) Pressure:

$$p(x, t) = j \frac{\rho c}{A} \frac{\sin[\Omega(l-x)/c]}{\cos(\Omega l/c)} U_g(\Omega)e^{j\Omega t}$$

where  $U_g(\Omega)e^{j\Omega t}$  denotes volume velocity at  $x = 0$

# SOLUTION FOR A LOSSLESS TUBE

Under the assumptions/conditions:

- No friction along the walls of the tube
- At the open end of the tube, there are no variations in air pressure, i.e.  $p(l, t) = 0$
- Volume velocity at  $x = 0$ :  $u(0, t) = U_g(\Omega)e^{j\Omega t}$

▷ Volume velocity:

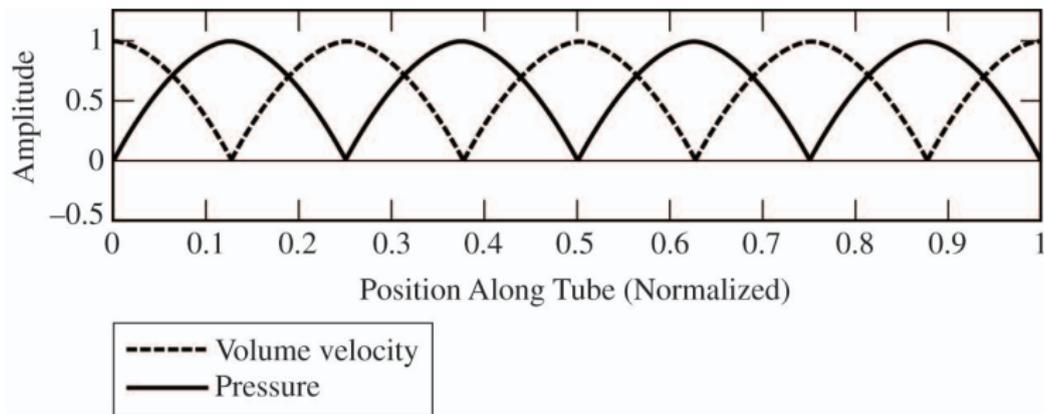
$$u(x, t) = \frac{\cos[\Omega(l-x)/c]}{\cos(\Omega l/c)} U_g(\Omega)e^{j\Omega t}$$

▷ (Incremental) Pressure:

$$p(x, t) = j \frac{\rho c}{A} \frac{\sin[\Omega(l-x)/c]}{\cos(\Omega l/c)} U_g(\Omega)e^{j\Omega t}$$

where  $U_g(\Omega)e^{j\Omega t}$  denotes volume velocity at  $x = 0$

# VELOCITY AND PRESSURE ARE “ORTHOGONAL”



# INPUT/OUTPUT VOLUME VELOCITY

At  $x = l$

$$u(l, t) = \frac{1}{\cos(\Omega l/c)} U_g(\Omega) e^{j\Omega t}$$

Then, the frequency response  $V(\Omega)$  is:

$$V(\Omega) = \frac{U(l, \Omega)}{U_g(\Omega)} = \frac{1}{\cos(\Omega l/c)}$$

providing resonances of infinite amplitudes at frequencies:

$$\Omega_k = (2k + 1) \frac{\pi c}{2l}, \quad k = 0, 1, 2, \dots$$

Example: if  $l = 35\text{cm}$ ,  $c = 350\text{ m/s}$ , then  $f_k = 250, 750, 1250, \dots$  Hz.

# INPUT/OUTPUT VOLUME VELOCITY

At  $x = l$

$$u(l, t) = \frac{1}{\cos(\Omega l/c)} U_g(\Omega) e^{j\Omega t}$$

Then, the frequency response  $V(\Omega)$  is:

$$V(\Omega) = \frac{U(l, \Omega)}{U_g(\Omega)} = \frac{1}{\cos(\Omega l/c)}$$

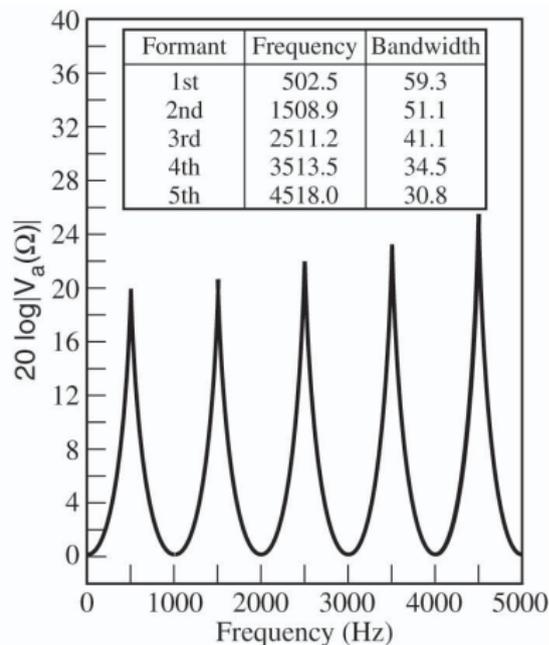
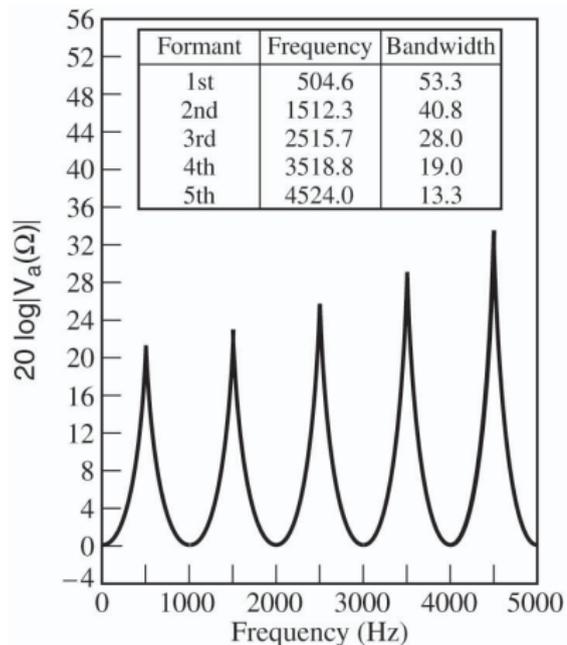
providing resonances of infinite amplitudes at frequencies:

$$\Omega_k = (2k + 1) \frac{\pi c}{2l}, \quad k = 0, 1, 2, \dots$$

Example: if  $l = 35\text{cm}$ ,  $c = 350\text{ m/s}$ , then  $f_k = 250, 750, 1250, \dots$  Hz.

# UNIFORM TUBE: BEING REALISTIC

Energy loss due to the wall vibration (left) and with viscous and thermal loss (right)[1]:

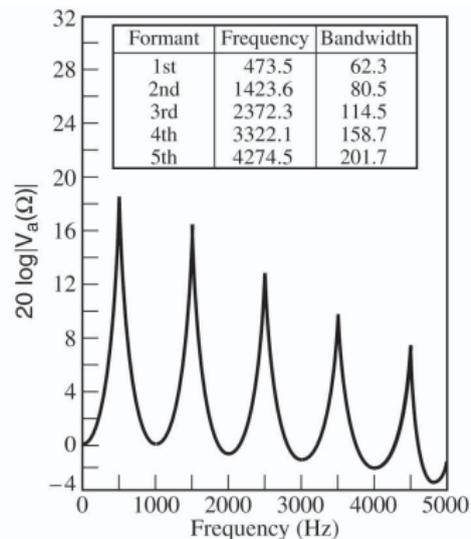


# UNIFORM TUBE: BEING MORE REALISTIC

Sound radiation at the lips, as an acoustic impedance:

$$Z_r(\Omega) = \frac{P(l, \Omega)}{U(l, \Omega)}$$

All the previous losses, plus radiation loss[1]:

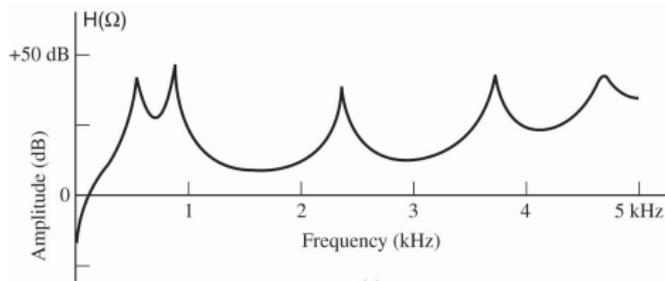


# PRESSURE-TO-VOLUME VELOCITY FREQUENCY RESPONSE

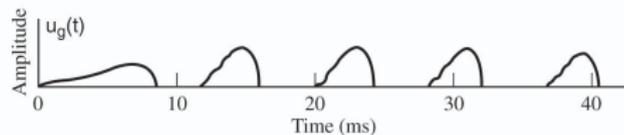
Since we measure pressure at the lips:

$$H(\Omega) = \frac{P(l, \Omega)}{U_g(\Omega)} = Z_r(\Omega)V(\Omega)$$

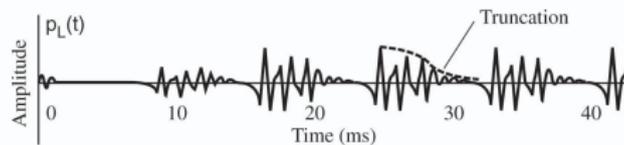
# NUMERICAL SIMULATIONS FOR /o/[1]



(a)



(b)

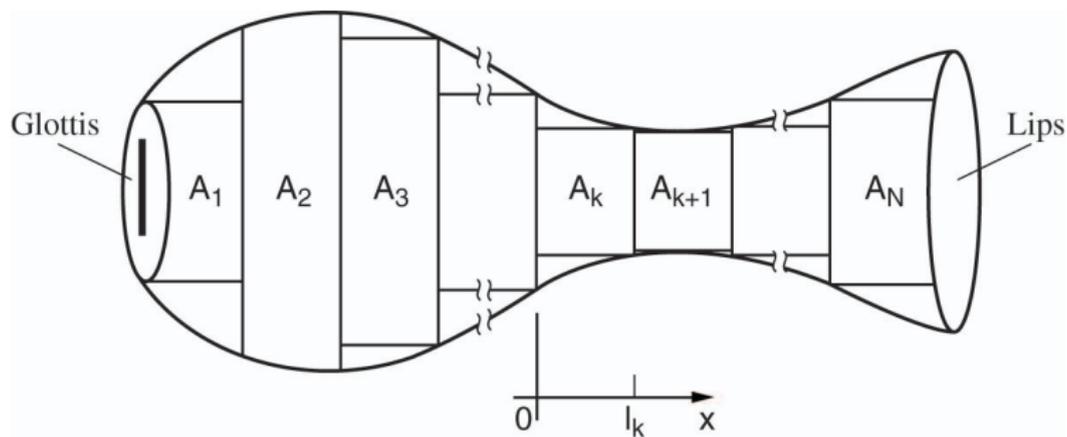


(c)

# OUTLINE

- 1 PHYSICS OF SOUND
- 2 UNIFORM TUBE MODEL
- 3 CONCATENATING N UNIFORM TUBES**
- 4 GLOTTAL FLOW DERIVATIVE
- 5 VOCAL FOLD/VOCAL TRACT INTERACTION
- 6 ACKNOWLEDGMENTS
- 7 REFERENCES

# CONCATENATING LOSSLESS UNIFORM TUBES



Reflection coefficient:

$$r_k = \frac{A_{k+1} - A_k}{A_{k+1} + A_k}$$

# DISCRETIZING THE CONTINUOUS-SPACE TUBE

- Impulse response of  $N$  lossless concatenated tubes with total length  $l$ :

$$h(t) = b_0\delta(t - N\tau) + \sum_{k=1}^{\infty} b_k\delta(t - N\tau - k2\tau)$$

where  $\tau = \frac{\Delta x}{c}$  and  $\Delta x = \frac{l}{N}$

- Frequency response:

$$H(\Omega) = \sum_{k=0}^{\infty} b_k e^{-j\Omega 2k\tau}$$

- Observe that:

$$H\left(\Omega + \frac{2\pi}{2\tau}\right) = H(\Omega)$$

# DISCRETIZING THE CONTINUOUS-SPACE TUBE

- Impulse response of  $N$  lossless concatenated tubes with total length  $l$ :

$$h(t) = b_0\delta(t - N\tau) + \sum_{k=1}^{\infty} b_k\delta(t - N\tau - k2\tau)$$

where  $\tau = \frac{\Delta x}{c}$  and  $\Delta x = \frac{l}{N}$

- Frequency response:

$$H(\Omega) = \sum_{k=0}^{\infty} b_k e^{-j\Omega 2k\tau}$$

- Observe that:

$$H\left(\Omega + \frac{2\pi}{2\tau}\right) = H(\Omega)$$

# DISCRETIZING THE CONTINUOUS-SPACE TUBE

- Impulse response of  $N$  lossless concatenated tubes with total length  $l$ :

$$h(t) = b_0\delta(t - N\tau) + \sum_{k=1}^{\infty} b_k\delta(t - N\tau - k2\tau)$$

where  $\tau = \frac{\Delta x}{c}$  and  $\Delta x = \frac{l}{N}$

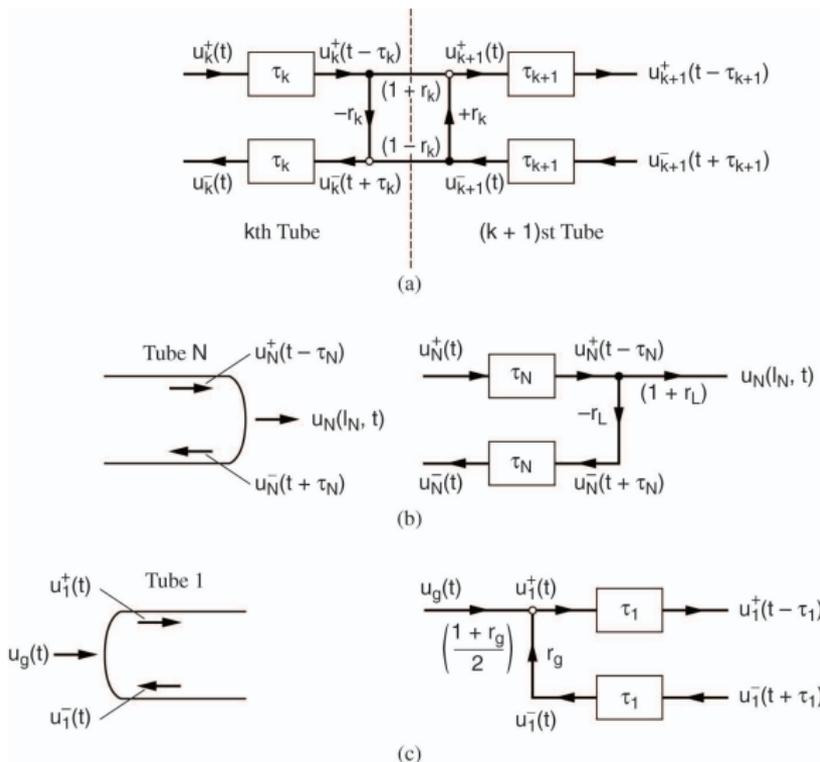
- Frequency response:

$$H(\Omega) = \sum_{k=0}^{\infty} b_k e^{-j\Omega 2k\tau}$$

- Observe that:

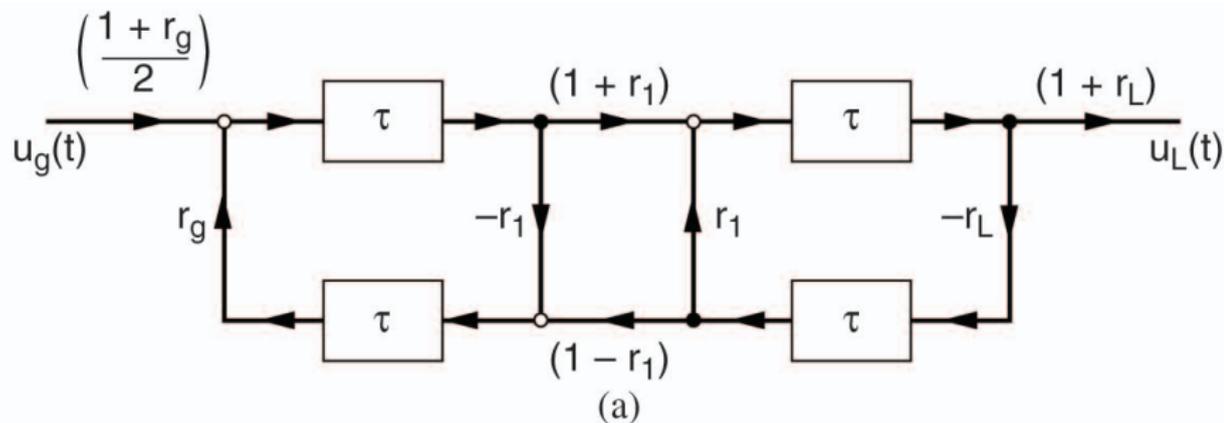
$$H\left(\Omega + \frac{2\pi}{2\tau}\right) = H(\Omega)$$

# SIGNAL FLOW GRAPHS



(a) two concatenated tubes, (b) lip boundary condition, (c) glottal boundary condition

# FOR A LOSSLESS TWO-TUBE MODEL



Transfer function relating the volume velocity at the lips to the glottis:

$$V(s) = \frac{be^{-s2\tau}}{1 + a_1e^{-s2\tau} + a_2e^{-s4\tau}}$$

with  $a_1 = r_1r_g + r_1r_L$ ,  $a_2 = r_Lr_g$  and  $b = 0.5(1+r_g)(1+r_L)(1+r_1)$   
 (Show me this)

# DISCRETE-TIME LOSSLESS MODELS

- **Two cubes:** By setting  $z = e^{s2\tau}$ , then:

$$V(z) = \frac{bz^{-1}}{1 + a_1z^{-1} + a_2z^{-2}}$$

- **N cubes:**

$$V(z) = \frac{Az^{-N/2}}{1 + \sum_{k=1}^N a_k z^{-k}}$$

# DISCRETE-TIME LOSSLESS MODELS

- **Two cubes:** By setting  $z = e^{s2\tau}$ , then:

$$V(z) = \frac{bz^{-1}}{1 + a_1z^{-1} + a_2z^{-2}}$$

- **N cubes:**

$$V(z) = \frac{Az^{-N/2}}{1 + \sum_{k=1}^N a_k z^{-k}}$$

# CHOOSING THE NUMBER OF TUBE ELEMENTS

## Question:

If a vocal tract has length  $l = 17.5 \text{ cm}$  and the speed of sound  $c = 350 \text{ m/s}$ , how many tubes,  $N$ , do we need to cover a bandwidth of  $5000 \text{ Hz}$ ?

Answer:  $N = 10$

# CHOOSING THE NUMBER OF TUBE ELEMENTS

## Question:

If a vocal tract has length  $l = 17.5 \text{ cm}$  and the speed of sound  $c = 350 \text{ m/s}$ , how many tubes,  $N$ , do we need to cover a bandwidth of  $5000 \text{ Hz}$ ?

**Answer:**  $N = 10$

# COMPLETE DISCRETE-TIME MODEL FROM N TUBES

Discrete-time pressure-to-volume velocity frequency response:

$$H(z) = R(z)V(Z)$$

where  $R(z) \approx 1 - \alpha z^{-1}$  and  $V(z)$  is an all-pole model.  
And for the speech signal (voiced case):

$$X(z) = A_v G(z)H(z)$$

with  $A_v$  to control loudness and  $G(z)$  being the z-transform of the glottal flow input.

or

$$X(z) = A_v G(z) \frac{1 - \alpha z^{-1}}{1 + \sum_{k=1}^N a_k z^{-k}}$$

# COMPLETE DISCRETE-TIME MODEL FROM N TUBES

Discrete-time pressure-to-volume velocity frequency response:

$$H(z) = R(z)V(z)$$

where  $R(z) \approx 1 - \alpha z^{-1}$  and  $V(z)$  is an all-pole model.  
And for the speech signal (voiced case):

$$X(z) = A_v G(z) H(z)$$

with  $A_v$  to control loudness and  $G(z)$  being the z-transform of the glottal flow input.

or

$$X(z) = A_v G(z) \frac{1 - \alpha z^{-1}}{1 + \sum_{k=1}^N a_k z^{-k}}$$

# GLOTTAL WAVEFORM MODEL

A typical glottal flow waveform over one cycle is modeled as:

$$g[n] = (b^{-n}u[-n]) \star (b^{-n}u[-n])$$

which has as z-transform:

$$G(z) = \frac{1}{(1 - \beta z)^2}$$

So for a *voiced* frame:

$$X(z) = A_v \frac{(1 - az^{-1})}{(1 - bz)^2 (1 + \sum_{k=1}^N a_k z^{-k})}$$

# GLOTTAL WAVEFORM MODEL

A typical glottal flow waveform over one cycle is modeled as:

$$g[n] = (b^{-n}u[-n]) \star (b^{-n}u[-n])$$

which has as z-transform:

$$G(z) = \frac{1}{(1 - \beta z)^2}$$

So for a *voiced* frame:

$$X(z) = A_v \frac{(1 - az^{-1})}{(1 - bz)^2 (1 + \sum_{k=1}^N a_k z^{-k})}$$

# MODELING OTHER STATES

- **For noisy inputs:**

$$X(z) = A_n U(z) V(z) R(z)$$

- **For impulsive sounds:**

$$X(z) = A_i V(z) R(z)$$

- **being more general:**

$$X(z) = A \frac{(1 - az^{-1}) \prod_{k=1}^{M_i} (1 - c_k z^{-1}) \prod_{k=1}^{M_o} (1 - d_k z)}{(1 - bz)^2 (1 - \sum_{k=1}^N a_k z^{-k})}$$

# MODELING OTHER STATES

- **For noisy inputs:**

$$X(z) = A_n U(z) V(z) R(z)$$

- **For impulsive sounds:**

$$X(z) = A_i V(z) R(z)$$

- **being more general:**

$$X(z) = A \frac{(1 - az^{-1}) \prod_{k=1}^{M_i} (1 - c_k z^{-1}) \prod_{k=1}^{M_o} (1 - d_k z)}{(1 - bz)^2 (1 - \sum_{k=1}^N a_k z^{-k})}$$

# MODELING OTHER STATES

- For noisy inputs:

$$X(z) = A_n U(z) V(z) R(z)$$

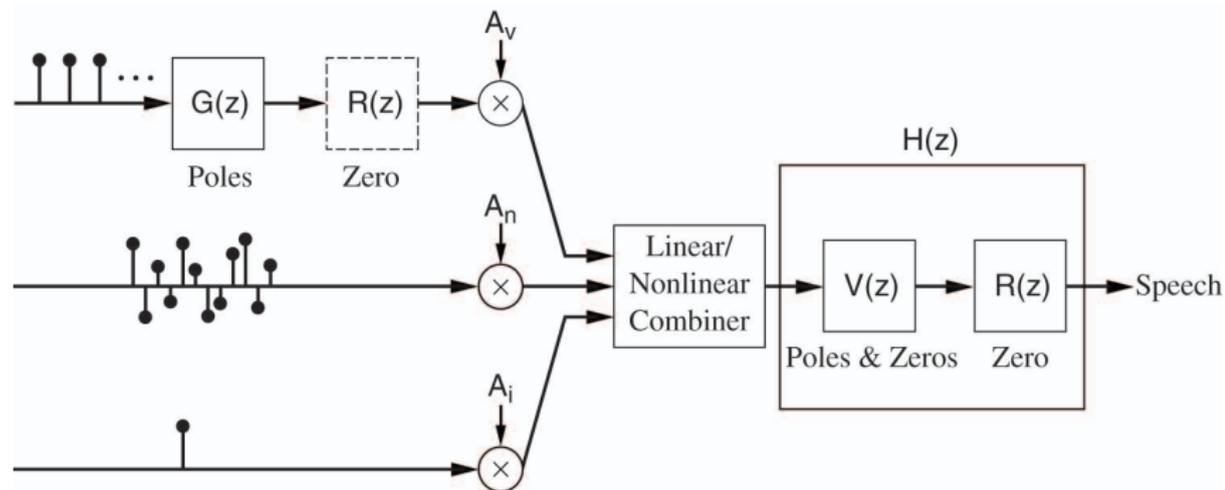
- For impulsive sounds:

$$X(z) = A_i V(z) R(z)$$

- being more general:

$$X(z) = A \frac{(1 - az^{-1}) \prod_{k=1}^{M_i} (1 - c_k z^{-1}) \prod_{k=1}^{M_o} (1 - d_k z)}{(1 - bz)^2 (1 - \sum_{k=1}^N a_k z^{-k})}$$

# AN OVERVIEW THEN



# OUTLINE

- 1 PHYSICS OF SOUND
- 2 UNIFORM TUBE MODEL
- 3 CONCATENATING N UNIFORM TUBES
- 4 GLOTTAL FLOW DERIVATIVE**
- 5 VOCAL FOLD/VOCAL TRACT INTERACTION
- 6 ACKNOWLEDGMENTS
- 7 REFERENCES

# GLOTTAL FLOW DERIVATIVE

Since speech signals,  $x(t)$  can be obtained in general by:

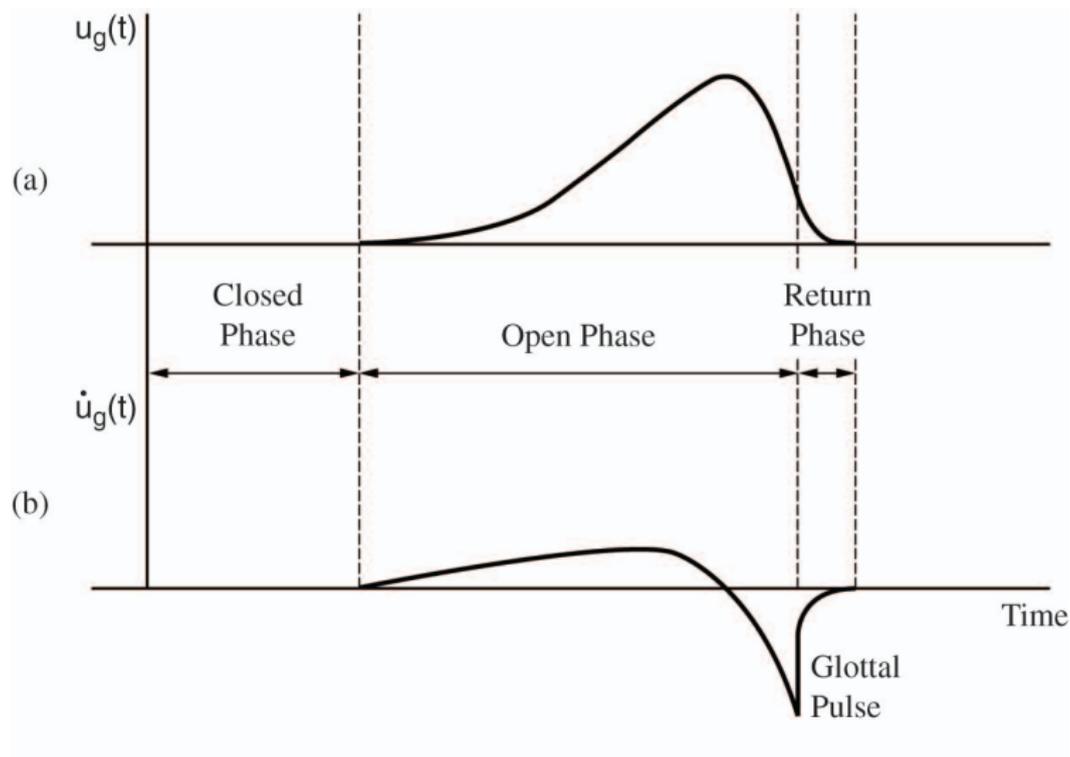
$$x(t) \approx A \frac{d}{dt} [u_g(t) \star v(t)]$$

and because:

$$A \frac{d}{dt} [u_g(t) \star v(t)] = A \left[ \frac{d}{dt} u_g(t) \right] \star v(t)$$

we usually consider the derivative  $\frac{d}{dt} u_g(t)$  as input to the system, which is referred to as *Glottal Flow Derivative*

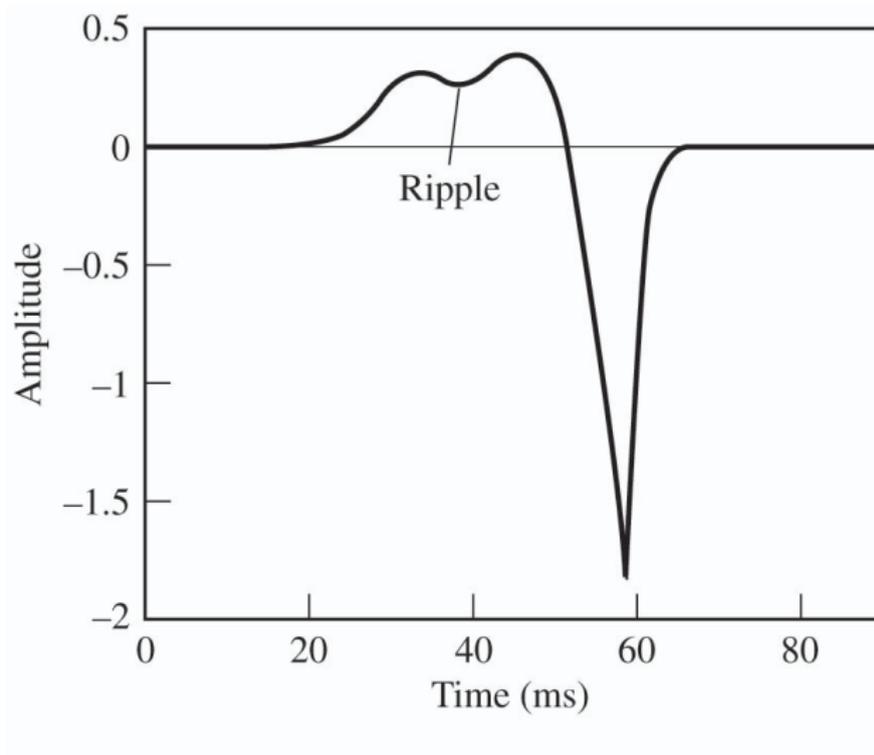
# GLOTTAL FLOW AND ITS DERIVATIVE



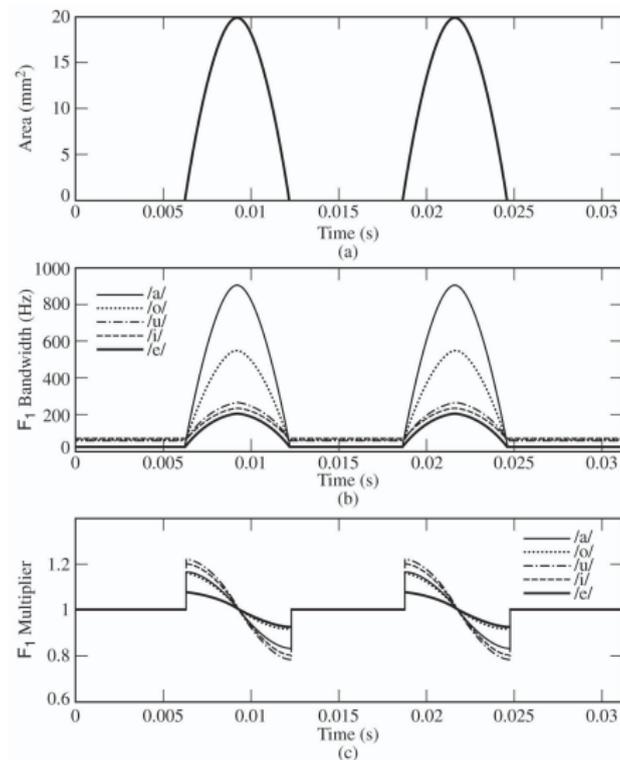
# OUTLINE

- 1 PHYSICS OF SOUND
- 2 UNIFORM TUBE MODEL
- 3 CONCATENATING N UNIFORM TUBES
- 4 GLOTTAL FLOW DERIVATIVE
- 5 VOCAL FOLD/VOCAL TRACT INTERACTION**
- 6 ACKNOWLEDGMENTS
- 7 REFERENCES

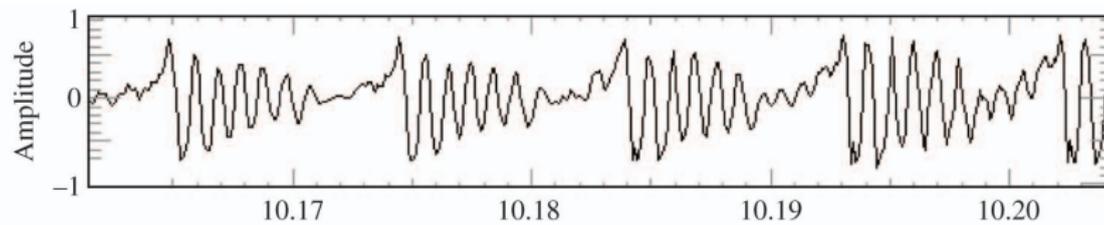
# RIPPLE IN THE GLOTTAL FLOW DERIVATIVE?



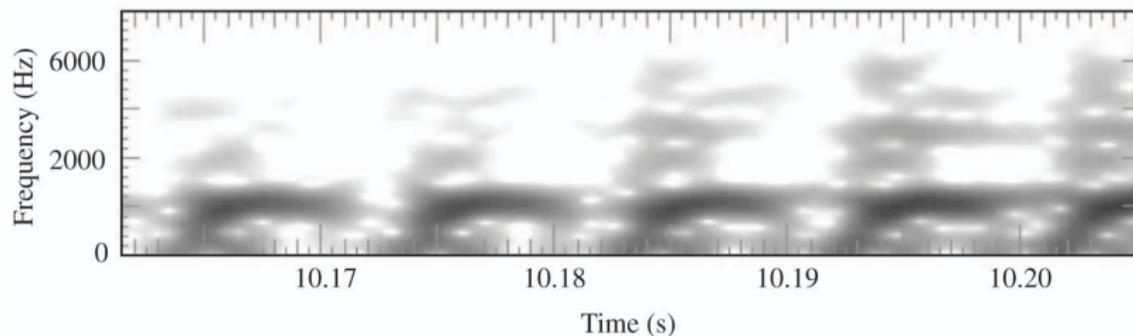
# REGARDING THE FIRST FORMANT [2]



# TRUNCATION EFFECT - AGAIN



(a)



(b)

# OUTLINE

- 1 PHYSICS OF SOUND
- 2 UNIFORM TUBE MODEL
- 3 CONCATENATING N UNIFORM TUBES
- 4 GLOTTAL FLOW DERIVATIVE
- 5 VOCAL FOLD/VOCAL TRACT INTERACTION
- 6 ACKNOWLEDGMENTS**
- 7 REFERENCES

# ACKNOWLEDGMENTS

Most, if not all, figures in this lecture are coming from the book:

**T. F. Quatieri:** Discrete-Time Speech Signal Processing,  
principles and practice  
2002, Prentice Hall

and have been used after permission from Prentice Hall

# OUTLINE

- 1 PHYSICS OF SOUND
- 2 UNIFORM TUBE MODEL
- 3 CONCATENATING N UNIFORM TUBES
- 4 GLOTTAL FLOW DERIVATIVE
- 5 VOCAL FOLD/VOCAL TRACT INTERACTION
- 6 ACKNOWLEDGMENTS
- 7 REFERENCES**



M. Portnoff, *A Quasi-One-Dimensional Digital Simulation for the Time-Varying Vocal Tract*.  
PhD thesis, Massachusetts Institute of Technology, May 1973.



C. Jankowski, *Fine Structure Features for Speaker Identification*.  
PhD thesis, Massachusetts Institute of Technology, Dept. of EE and CS, June 1996.



# Τέλος Ενότητας



Ευρωπαϊκή Ένωση  
Πρωτόκολλο Κοινωνίας Τεχνών



# Χρηματοδότηση

- Το παρόν εκπαιδευτικό υλικό έχει αναπτυχθεί στα πλαίσια του εκπαιδευτικού έργου του διδάσκοντα.
- Το έργο «**Ανοικτά Ακαδημαϊκά Μαθήματα στο Πανεπιστήμιο Κρήτης**» έχει χρηματοδοτήσει μόνο τη αναδιαμόρφωση του εκπαιδευτικού υλικού.
- Το έργο υλοποιείται στο πλαίσιο του Επιχειρησιακού Προγράμματος «Εκπαίδευση και Δια Βίου Μάθηση» και συγχρηματοδοτείται από την Ευρωπαϊκή Ένωση (Ευρωπαϊκό Κοινωνικό Ταμείο) και από εθνικούς πόρους.



**Σημειώματα**

# Σημείωμα αδειοδότησης

- Το παρόν υλικό διατίθεται με τους όρους της άδειας χρήσης Creative Commons Αναφορά, Μη Εμπορική Χρήση, Όχι Παράγωγο Έργο 4.0 [1] ή μεταγενέστερη, Διεθνής Έκδοση. Εξαιρούνται τα αυτοτελή έργα τρίτων π.χ. φωτογραφίες, διαγράμματα κ.λ.π., τα οποία εμπεριέχονται σε αυτό και τα οποία αναφέρονται μαζί με τους όρους χρήσης τους στο «Σημείωμα Χρήσης Έργων Τρίτων».

[1] <http://creativecommons.org/licenses/by-nc-nd/4.0/>



- Ως **Μη Εμπορική** ορίζεται η χρήση:
  - που δεν περιλαμβάνει άμεσο ή έμμεσο οικονομικό όφελος από την χρήση του έργου, για το διανομέα του έργου και αδειοδόχο
  - που δεν περιλαμβάνει οικονομική συναλλαγή ως προϋπόθεση για τη χρήση ή πρόσβαση στο έργο
  - που δεν προσπορίζει στο διανομέα του έργου και αδειοδόχο έμμεσο οικονομικό όφελος (π.χ. διαφημίσεις) από την προβολή του έργου σε διαδικτυακό τόπο
- Ο δικαιούχος μπορεί να παρέχει στον αδειοδόχο ξεχωριστή άδεια να χρησιμοποιεί το έργο για εμπορική χρήση, εφόσον αυτό του ζητηθεί.

# Σημείωμα Αναφοράς

Copyright Πανεπιστήμιο Κρήτης, Στυλιανού Ιωάννης. «Ψηφιακή Επεξεργασία Φωνής. Ακουστική Ανάλυση Παραγωγής Φωνής». Έκδοση: 1.0. Ηράκλειο/ Ρέθυμνο 2015. Διαθέσιμο από τη δικτυακή διεύθυνση: <http://www.csd.uoc.gr/~hy578>

# Διατήρηση Σημειωμάτων

Οποιαδήποτε αναπαραγωγή ή διασκευή του υλικού θα πρέπει να συμπεριλαμβάνει:

- το Σημείωμα Αναφοράς
- το Σημείωμα Αδειοδότησης
- τη δήλωση Διατήρησης Σημειωμάτων
- το Σημείωμα Χρήσης Έργων Τρίτων (εφόσον υπάρχει)

μαζί με τους συνοδευόμενους υπερσυνδέσμους.

# Σημείωμα Χρήσης Έργων Τρίτων

Το Έργο αυτό κάνει χρήση των ακόλουθων έργων:

## **Εικόνες/Σχήματα/Διαγράμματα/Φωτογραφίες**

Εικόνες/σχήματα/διαγράμματα/φωτογραφίες που περιέχονται σε αυτό το αρχείο προέρχονται από το βιβλίο:

Τίτλος: *Discrete-time Speech Signal Processing: Principles and Practice*

Prentice-Hall signal processing series, ISSN 1050-2769

Συγγραφέας: Thomas F. Quatieri

Εκδότης: Prentice Hall PTR, 2002

ISBN: 013242942X, 9780132429429

Μέγεθος: 781 σελίδες

και αναπαράγονται μετά από άδεια του εκδότη.