SINUSOIDAL MODELING

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A SIMPLE VIEW



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Downward-looking into the larynx: Vocal Folds



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GLOTTAL AIRFLOW VELOCITY



VOCAT TRACT SHAPES



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EXAMPLE

Let the excitation of vocal tract, h[n], be:

$$u[n] = g[n] \star p[n]$$

then, the output speech, $x[n, \tau]$, is given by:

nd

$$x[n,\tau] = w[n,\tau] \{h[n] \star (g[n] \star p[n])\}$$

$$X(\omega,\tau) = \underbrace{\mathbb{P}}_{k=-\infty}^{\infty} H(\omega_k) G(\omega_k) W(\omega - \omega_k,\tau)$$

and

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HARMONICS AND FORMANTS



• Sinusoidal Model:

$$x(t) = \sum_{k=-K}^{K} \gamma_k e^{j2\pi f_k t}$$

• Special case, Harmonic Model:

$$x(t) = \sum_{k=-K}^{K} \gamma_k e^{j2\pi k f_0 t}$$

• Estimation of parameters (Linear approach):

$$\gamma = \mathcal{F}_{f_k} \mathbf{s}$$

• Model Evaluation, Mean-Squared Error (MSE):

$$\epsilon = \int_{w} |s(t) - x(t)|^2 dt$$

• Sinusoidal Model:

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Source-Filter with Sinusoids

• Source:

$$u(t) = \sum_{k=-K(t)}^{K(t)} \alpha_k(t) e^{j\phi_k(t)}$$

where:

$$\phi_k(t) = \int_0^t \Omega_k(\sigma) d\sigma + \phi_k$$

• Filter: $h(t, \tau)$ with Fourier Transform (FT): $H(t, \Omega) = M(t, \Omega)e^{j\Phi(t, \Omega)}$

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Source-Filter with Sinusoids

$$s(t) = \sum_{k=1-\mathcal{K}(t)}^{\mathcal{K}(t)} A_k(t) e^{j heta_k(t)}$$

where:

$$\begin{array}{lll} \mathcal{A}_k(t) &=& \alpha_k(t) \mathcal{M}\left[t, \Omega_k(t)\right] \\ \theta_k(t) &=& \phi_k(t) + \Phi\left[t, \Omega_k(t)\right] \\ &=& \int_0^t \Omega_k(\sigma) d\sigma + \Phi\left[t, \Omega_k(t)\right] + \phi_k \end{array}$$

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We assume stationarity inside the analysis window:

$$egin{array}{rcl} A_k(t)&=&A_k\ \Omega_k(t)&=&\Omega_k\ K(t)&=&K \end{array}$$

which leads to:

$$\theta_k(t) = \Omega_k(t-t_l) + \theta_k$$

and to:

$$s(t) = \sum_{k=-K}^{K} A_k e^{j\theta_k} e^{j\Omega_k(t-t_l)} \quad t_l - \frac{T}{2} \le t \le t_l + \frac{T}{2}$$

In discrete time:

$$s[n] = \sum_{k=-K}^{K} \gamma_k e^{j\omega_k n} - \frac{N_w - 1}{2} \le n \le \frac{N_w - 1}{2}$$

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and to:

 $s(t) = \sum_{k=-K}^{K} \underbrace{A_k e^{j\theta_k} e^{j\Omega_k(t-t_l)}}_{k=-K} t_l - \frac{T}{2} \le t \le t_l + \frac{T}{2}$ In discrete time: $s[n] = \sum_{k=-K}^{K} \gamma_k e^{j\omega_k n} - \frac{N_w - 1}{2} \le n \le \frac{N_w - 1}{2}$

MEAN-SQUARED ERROR

Given the original measured waveform, y[n] and the synthetic speech waveform, s[n], estimate the unknown parameters A'_k , ω'_k , and θ'_k by minimizing the MSE criterion:

$$\epsilon' = \sum_{n=-(N_w-1)/2}^{n=(N_w-1)/2} |y[n] - s[n]|^2$$

which can be written as:

$$\epsilon' = \sum_{n=-(N_w-1)/2}^{n=(N_w-1)/2} |y[n]|^2 + N_w \sum_{k=1}^{K'} \left(\left| Y(\omega_k') - \gamma_k' \right|^2 - |Y(\omega_k')|^2 \right)$$

which can be reduced further to:

$$\epsilon^{l} = \sum_{n=-(N_{w}-1)/2}^{n=(N_{w}-1)/2} |y[n]|^{2} - N_{w} \sum_{k=1}^{K^{l}} |Y(\omega_{k}^{l})|^{2}$$

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- Karhunen-Loève expansion allows constructing a random process from harmonic sinusoids with uncorrelated complex amplitudes.
- Estimated power spectrum should not vary "too much" over consecutive frequencies.

Following the above necessary constraints, for unvoiced speech, and for a window width to be *at least* 20ms, an 100 Hz harmonic structure provides good results.

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SINUSOIDAL ANALYSIS: PEAK PICKING



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SINUSOIDAL SYNTHESIS: OLA, A SIMPLE SOLUTION



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PROBLEM OF FREQUENCY MATCHING



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Outline Speech Production Modulators Sinusoidal Modeling Harmonic Modeling HNM2 or QHM References

FRAME-TO-FRAME PEAK MATCHING



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THE BIRTH/DEATH PROCESS



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A BIRTH/DEATH PROCESS IN SPEECH



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Amplitude and Phase Interpolation

• Linear amplitude interpolation model:

$$A'_{k}[n] = A'_{k} + \left(A'^{+1}_{k} - A'_{k}\right)\left(\frac{n}{L}\right) \quad n = 0, 1, 2, \cdots, L - 1$$

• Cubic Phase interpolation model

$$\theta(t) = \zeta + \gamma t + \alpha t^2 + \beta t^3 + 2 \Box M$$

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BLOCK DIAGRAM OF THE SYNTHESIS SYSTEM



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Synthesis: Reconstruction Example



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HARMONIC MODEL

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Sinusoidal Modeling

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BRIEF OVERVIEW OF HNM

- HNM is a pitch-synchronous harmonic plus noise representation of the speech signal.
- Speech spectrum is divided into a low and a high band delimited by the so-called maximum voiced frequency.
- The low band of the spectrum (below the maximum voiced frequency) is represented solely by harmonically related sine waves.
- The upper band is modeled as a noise component modulated by a time-domain amplitude envelope.
- HNM allows high-quality copy synthesis and prosodic modifications.

HNM IN EQUATIONS

• Harmonic part:

$$h(t) = \sum_{k=-L(t)}^{L(t)} A_k(t) e^{j k \omega_0(t) t}$$
$$n(t) = e(t) [v(\tau, t) \star b(t)]$$
$$s(t) = h(t) + n(t)$$

• Noise part:

• Speech:

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PERIODIC PART

• HNM₁: Sum of exponential functions without slope

$$h_1[n] = \sum_{k=-L(n_a^i)}^{L(n_a^i)} a_k(n_a^i) e^{j2\pi k f_0(n_a^i)(n-n_a^i)}$$

• HNM₂: Sum of exponential function with complex slope

$$h_2[n] = \Re \left\{ \sum_{k=1}^{L(n_a^i)} A_k(n) \exp^{j2\pi k f_0(n_a^i)(n-n_a^i)} \right\}$$

where

$$A_k(n) = a_k(n_a^i) + (n - n_a^i)b_k(n_a^i)$$

with $a_k(n_a^i)$, $b_k(n_a^i)$ to be complex numbers (amplitude and slope respectively). \Re denotes taking the real part.

PERIODIC PART

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with $a_k(n_a^i)$, $b_k(n_a^i)$ to be complex numbers (amplitude and slope respectively). \Re denotes taking the real part.

PERIODIC PART continuing

• HNM₃: Sum of sinusoids with time-varying real amplitudes

$$h_3[n] = \sum_{k=0}^{L(n_a^i)} a_k(n) cos(\varphi_k(n))$$

where

$$\begin{aligned} a_k(n) &= c_{k0} + c_{k1} (n - n_a^i)^1 + \dots + c_{kp} (n - n_a^i)^{p(n)} \\ \varphi_k(n) &= \epsilon_k + 2\pi \, k\zeta (n - n_a^i) \end{aligned}$$

where p(n) is the order of the amplitude polynomial, which is, in general, a time-varying parameter.

Residual (Noise) part

The non-periodic part is just the *residual* signal obtained by subtracting the periodic-part (harmonic part) from the original speech signal in the time-domain

$$r[n] = s[n] - h[n]$$

where h[n] is either $h_1[n]$, $h_2[n]$, or $h_3[n]$.

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AMPLITUDES AND PHASES ESTIMATION

Having f_0 estimated for voiced frames, amplitudes and phases are estimated by minimizing the criterion:

$$\epsilon = \sum_{\substack{n=n_a^i - N \\ n=n_a^i - N}}^{n_a^i + N} w^2[n](s[n] - \hat{h}[n])^2$$

where $n_a^i = n_a^{i-1} + P(n_a^{i-1})$, and $P(n_a^{i-1})$ denotes the pitch period at n_a^{i-1} .

- for HNM₁ and HNM₂, this criterion has a quadratic form and is solved by inverting an over-determined system of linear equations.
- For HNM₃, however,a non-linear system of equations has to be solved.

The residual signal r[n] is estimated by

$$\hat{r}[n] = s[n] - \hat{h}[n]$$

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TIME DOMAIN CHARACTERISTICS OF $\hat{r}[n]$



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VARIANCE OF THE RESIDUAL SIGNAL

The variance of the residual signal is given as:

$$E(\mathbf{rr}^{h}) = \mathbf{I} - \mathbf{WP}(\mathbf{P}^{h}\mathbf{W}^{h}\mathbf{WP})^{-1}\mathbf{P}^{h}\mathbf{W}^{h}$$



MODELING ERROR



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MODELING THE RESIDUAL SIGNAL

- Full bandwidth representation using a low-order (10th) AR filter
- Time-domain characteristics of the residual signal can be modeled using various functions



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TIME DOMAIN ENERGY MODULATION



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TRIANGULAR ENVELOPE



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SIGNAL ENVELOPE

There are many ways to obtain the "envelope" of a signal, as:

• Hilbert Transform (analytic signal)

• Low-pass local energy (energy envelope):

$$e[n] = \frac{1}{2N+1} \sum_{k=-N}^{N} |r[n-k]|$$

where r[n] denotes the residual signal.

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EXAMPLE OF ENERGY ENVELOPE

Example of Energy Envelope, with N = 7



The energy envelope can be efficiently parameterized with a few Fourier coefficients:

$$\hat{\mathbf{e}}[n] = \sum_{k=-L_e}^{L_e} A_k e^{j2\pi k (f_0/f_s)n}$$

where L_e is set to be 3 to 4

COMPARING TIME-DOMAIN MODULATIONS



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Sinusoidal Modeling

Sound Examples using HNM_1

 $\mathsf{Examples}$ with HNM_1 and $\mathsf{Maximum}$ Voiced frequency fixed at 4000 Hz

	Original	Triangular	Hilbert	Energy
Male	14		14	
Male				L]4
Female	口4			5
Female	C) 4	C)4		C) 7

Sound Examples using HNM_2

 $\mathsf{Examples}$ with HNM_2 and $\mathsf{Maximum}$ Voiced frequency fixed at 4000 Hz

	Original	Triangular	Hilbert	Energy
Male	14		14	
Male				L]4
Female	口4			5
Female	C) 4	C)4		C) 7

HNM_2

We recall that the HNM_2 is given by:

$$s(t) = \left(\sum_{k=-L}^{L} (a_k + tb_k)e^{2\pi jkf_0t}\right)w(t)$$

or in frequency domain:

$$S(f) = \sum_{k=-L}^{L} \left(a_k W(f - kf_0) + jb_k W'(f - kf_0) \right)$$

where W(f) is the Fourier Transform of window w(t)

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Frequency Domain properties of HNM_2

Let \vec{a}_k and \vec{b}_k denote the vectors corresponding respectively to the complex a_k and b_k and

let's decompose b_k into two components:

• one collinear to \vec{a}_k , and

• one perpendicular to \vec{a}_k .

Thus, \dot{b}_k is given by

$$\vec{b}_k = \rho_{1,k}\vec{a}_k + \rho_{2,k}\vec{a}_k^\perp,$$

where

$$\vec{a}_{k}^{\perp} = (-a_{k}^{\prime}, a_{k}^{R})^{T}$$
$$\rho_{1,k} = \frac{\langle \vec{a}_{k}, \vec{b}_{k} \rangle}{|\vec{a}_{k}|^{2}}$$
$$\rho_{2,k} = \frac{\langle \vec{a}_{k}^{\perp}, \vec{b}_{k} \rangle}{|\vec{a}_{k}|^{2}}$$

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Sinusoidal Modeling

FREQUENCY DOMAIN PROPERTIES OF HNM₂

Let \vec{a}_k and \vec{b}_k denote the vectors corresponding respectively to the complex a_k and b_k and let's decompose \vec{b}_k into two components:

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where

$$\vec{a}_{k}^{\perp} = (-a_{k}^{I}, a_{k}^{R})^{T}$$
$$\rho_{1,k} = \frac{\langle \vec{a}_{k}, \vec{b}_{k} \rangle}{|\vec{a}_{k}|^{2}}$$
$$\rho_{2,k} = \frac{\langle \vec{a}_{k}^{\perp}, \vec{b}_{k} \rangle}{|\vec{a}_{k}|^{2}}$$

 $\langle .\, ,. \rangle$ denotes the inner product between two vectors.

LET'S LOOK AT THE k^{th} COMPONENT

• The *kth* component can be written as:

$$S_k(f) = \sum_{k=0}^{\infty} k [W(f - kf_0) - \rho_{2,k}W'(f - kf_0) + j\rho_{1,k}W'(f - kf_0)]$$

 For small values of ρ_{2,k}, using a first order approximation of the Taylor series of W(f), we have:

$$W(f - kf_0) - \rho_{2,k}W'(f - kf_0) \approx W(f - kf_0 - \rho_{2,k})$$

• and then:

$$S_k(f) = [W(f - kf_0 - \rho_{2,k}) + j\rho_{1,k}W'(f - kf_0)]$$

• Then, HNM₂ becomes Quasi-Harmonic Model (QHM).

SENSITIVITY ON f_0



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T. F. Quatieri, Discrete-Time Speech Signal Processing.

Engewood Cliffs, NJ: Prentice Hall, 2002.

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